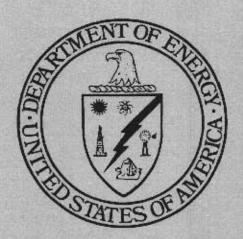


Sandia National Laboratories / New Mexico

PROPOSAL FOR NO FURTHER ACTION ENVIRONMENTAL RESTORATION PROJECT SITE 235, STORM DRAIN SYSTEM OUTFALL SITE OPERABLE UNIT 1309

June 1995

Environmental Restoration Project

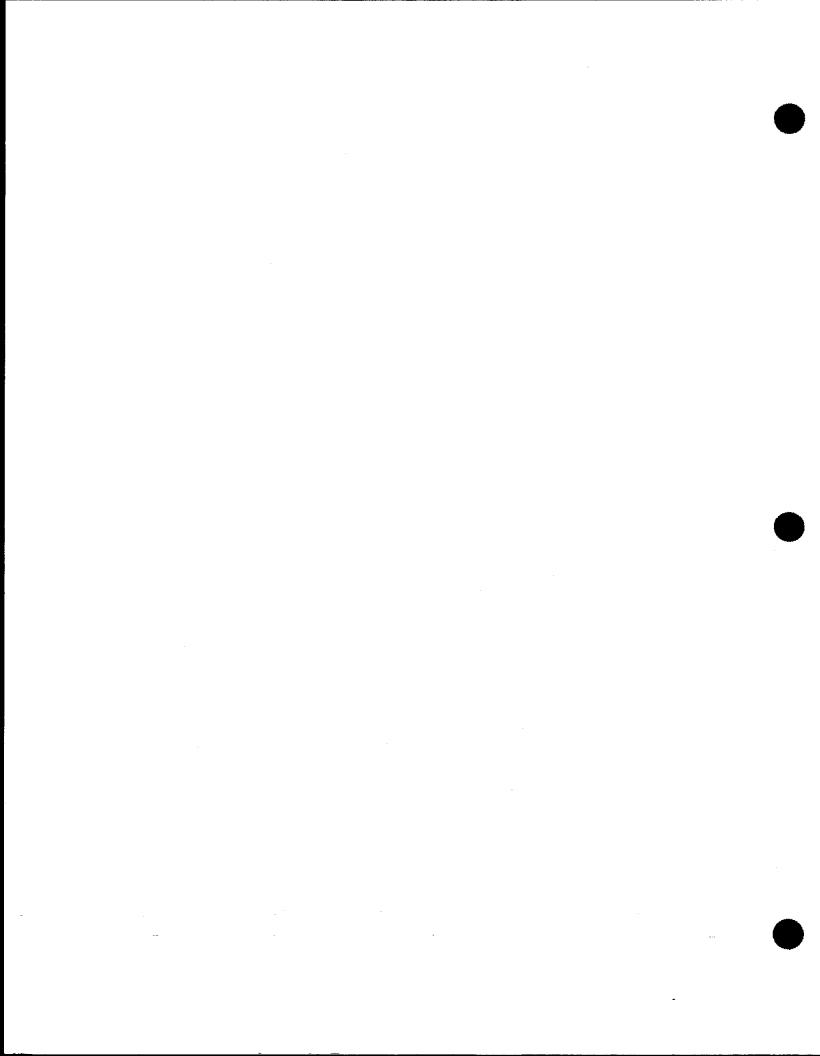


United States Department of Energy Albuquerque Operations Office

PROPOSAL FOR NO FURTHER ACTION

Site 235, Storm Drain System Outfall Site Operable Unit 1309

SANDIA NATIONAL LABORATORIES/NEW MEXICO



1. Introduction

1.1 ER Site Identification Number and Name

Sandia National Laboratories/New Mexico (SNL/NM) is proposing a risk-based no further action (NFA) decision for Environmental Restoration (ER) Site 235, Storm Drain System Outfall Site, Operable Unit (OU) 1309. ER Site 235 is listed in the Hazardous and Solid Waste Amendment (HSWA) Module IV (EPA August 1993) of the SNL/NM Resource Conservation and Recovery Act (RCRA) Hazardous Waste Management Facility Permit (NM5890110518) (EPA August 1992).

1.2 SNL/NM Risk-Based NFA Process

This proposal for a determination of an NFA decision has been prepared using the criteria presented in Section 4.5.3 of the SNL/NM Program Implementation Plan (PIP) (SNL/NM February 1994). Specifically, this proposal will "contain information demonstrating that this SWMU has never contained constituents of concern that may pose a threat to human health or the environment" [as proposed in the Code of Federal Regulations (CFR), Section 40 Part 264.51(a) (2)] (EPA July 1990). The HSWA Module IV contains the same requirements for an NFA demonstration:

Based on the results of the RFI [RCRA Facility Investigation] and other relevant information, the Permittee may submit an application to the Administrative Authority for a Class III permit modification under 40 CFR 270.42(c) to terminate the RFI/CMS [corrective measures study] process for a specific unit. This permit modification application must contain information demonstrating that there are no releases of hazardous waste including hazardous constituents from a particular SWMU at the facility that pose threats to human health and/or the environment, as well as additional information required in 40 CFR 270.42(c) (EPA August 1993).

For a risk-based proposal, an SWMU is eligible for an NFA determination if the NFA criterion established by the SNL/NM permit is met. This criterion, found in Section M.1 of the permit, is as follows: "[T]here are no releases of hazardous waste including hazardous constituents...that pose threats to human health and/or the environment..." This risk-base proposal contains information needed to make the NFA determination.

This proposal uses the technical approach which is the foundation for the SNL/NM corrective action process. The details of the SNL/NM technical approach are provided in Appendix C of the SNL/NM PIP (SNL/NM 1994). The first step in the technical approach is the data qualitative review step (the same step used to determine whether the SWMU is eligible for administrative-type NFA). Should significant uncertainties remain, the assessment of the SWMU continues with data collection.

At this site, sufficient data were not available to compare to established action levels or to develop site-specific action levels. Background soil samples were collected and analyzed to

develop upper tolerance limits (UTLs) for metals. Site-specific data were collected to compare to existing soil action levels (proposed Subpart S action levels) and UTLs. If site-specific concentrations exceeded the proposed Subpart S action levels or UTLs, then a risk assessment was performed. The site-specific concentrations were compared to the derived risk assessment action levels. Concentrations less than these action levels, either proposed Subpart S action levels, background UTLs, or derived risk-based values, triggered this NFA proposal for Site 235.

1.3 Local Setting

SNL/NM occupies 2,829 acres of land owned by the Department of Energy (DOE), with an additional 14,920 acres of land provided by land-use permits with Kirtland Air Force Base (KAFB), the United States Forest Service, the State of New Mexico, and the Isleta Indian Reservation. SNL/NM has been involved in nuclear weapons research, component development, assembly, testing, and other nuclear activities since 1945.

ER Site 235 (Figure 1) is located on land owned by DOE. It is located immediately downstream of a large spillway on the northeast side of Pennsylvania Avenue and south of the Skeet Range, at the point where the road comes off the north bank of the arroyo and descends into the channel. The flow moves in a confined channel after dropping down the energy dissipation structure.

Surficial deposits in the SNL/KAFB area lie within four geomorphic provinces, which in turn contain nine geomorphic subprovinces. Site 235 lies with in the Tijeras Arroyo subprovince. The Tijeras Arroyo subprovince is characterized by broad, west-sloping alluvial surfaces and the 50-meter-deep Tijeras Arroyo. The Tijeras Arroyo subprovince contains deposits derived from many sources, including granitic and sedimentary rocks of the Sandia Mountains, sedimentary and metamorphic rocks of the Manzanita Mountains, and sediments of the Upper Santa Fe Group.

2. History of the SWMU

2.1 Sources of Supporting Information

In support of the request for a risk-based with confirmatory sampling NFA decision for ER Site 235, a background study was conducted to collect available and relevant site information. Interviews were conducted with SNL/NM staff and contractors familiar with site operational history.

The following information sources were available for the use in the evaluation of ER Site 235:

- Confirmatory-sampling program conducted in September 1994
- Risk analysis for four metals and two radionuclides
- One surface radiation survey
- One unexploded ordnance/high explosives (UXO/HE) survey
- Interviews and personnel correspondence

• Historical aerial photographs spanning 40 years

2.2 Previous Audits, Inspections, and Findings

In November 1993, the Sandia ER staff recognized Site 235 as an SWMU. ER Site 235 was not listed as a potential release site based on the Comprehensive Environmental Assessment and Response Program (CEARP) interviews in 1985 (DOE September 1987). In addition, Site 235 was not included in the Environmental Protection Agency (EPA) RCRA Facility Assessment (RFA) in 1987 (EPA April 1987) and Site 235 was not included in the Hazard Ranking System (DOE September 1987).

2.3 Historical Operations

The outfall discharged industrial effluent and storm water from Technical Areas (TAs) I, II, and IV and tracts outside of the TAs. Currently, the outfall discharges only storm water. The specific constituents in the industrial effluent are not known. The possible contaminants include chromates, antifoulants, chromium, sodium hydroxide, hydrochloric acid, chromosulfuric acid, diesel, and other petroleum products. Mineral oil is also being considered a potential soil contaminant due to a recent release (June 1994) of mineral oil at a similar outfall, Site 232. This site is considerably larger than the other outfall sites. During the summer of 1994, the outfall has been reworked by the Air Force to stabilize it where Pennsylvania Avenue runs adjacent to it. The southern bank of the outfall channel was reworked and covered with soil, rock, and metal mesh.

3. Evaluation of Relevant Evidence

3.1 Unit Characteristics

The Storm Drain System Outfall is confined to the downstream natural drainage. All releases would be contained in this limited area.

3.2 Operating Practices

The outfall discharged industrial effluent and storm water from approximately 1978 to 1991.

3.3 Presence or Absence of Visual Evidence

The approximately 1,500-ft long outfall and the concrete energy dissipation structure are the only physical evidence of the outfall system. No discoloration of soils was observed during site reconnaissance and soil sampling activities.

3.4 Results of Previous Sampling/Surveys

In 1994, the site has been visually surveyed for surface indications of UXO/HE. No UXO/HE were found (SNL/NM 1994a). Also in 1994, a surface radiation survey was conducted on the entire site using an Eberline ESP-2 portable scaler, with an Eberline SPA-8

(2 inch X 2 inch sodium iodide) detector. A 30-second integrated count was performed at each proposed sample location, while scanning the detector over an area approximately 2 feet in radius around the sample location. The alarm was set at 1.3 times the background count rate. No alarms occurred during the survey. No surface anomalies were detected (SNL/NM 1994b).

3.5 Assessment of Gaps in Information

No environmental sampling data existed for Site 235. If contamination was present, potential constituents of concern (metals, radioactive constituents, and organic constituents), would be expected at shallow depths. Metals and radioactive constituents generally adsorb on soil and precipitate rather than remaining soluble. If organic constituents were introduced in the drainage, they should be detectable in surface or shallow subsurface soils.

3.6 Confirmatory Sampling

A surface (0-6 inches deep) and shallow subsurface (6-36 inches deep) soil sampling program was developed and implemented in September 1994. The Confirmatory Sampling and Analysis Plan (SAP) can be found in Appendix A. Those soil sample results exceeding an action level are summarized in Table 1. A complete list of "hits" or detections and quality assurance (QA) results can be found in Appendix B.

For health and safety purposes, a photoionization detector, OVM, was used throughout the field program. The OVM measured no anomalous vapor concentrations.

Surface and shallow subsurface soil samples were collected at the most likely locations of contamination. Three surface and three subsurface soil samples were collected along the northern side¹ of the outfall (Figure 1). Every sample was analyzed for metals², chromium⁴⁶, and total petroleum hydrocarbon (TPH). The three subsurface samples were analyzed for volatile organic compounds (VOCs). Four samples were analyzed for semivolatile organic compounds (SVOCs). As a general check for radioactive constituents, two samples were analyzed for tritium, and isotopic uranium and plutonium, and four samples were screened with in-house gamma spectroscopy.

3.6.1 Background Samples for Metals and Radioactive Constituents

UTLs for background metals were calculated from analyses of 24 samples collected in the vicinity of the 11 sites discussed in the SAP (Appendix A). UTLs or background 95th percentiles for background radionuclides were calculated from samples collected throughout KAFB (IT 1994). A discussion of background calculations and supporting data and analyses are included in Appendices C and D.

¹ Samples were not collected from the southern side because of the Air Force's rework of that area.

Although the target analyte list (TAL) metal analytes include calcium, magnesium, potassium, and sodium, these nontoxic, major cations are not included in the evaluation. They do not pose a significant environmental or human health risk regardless of concentration.

3.6.2 Organic Compounds

No analyses yielded positive detections of organic compounds. All detections were qualified with a "J", meaning detection below the reportable limit or a "B," meaning detected in the associated blank, or both. None of these qualified detections indicate significant contamination. No TPH was detected.

3.6.3 Metals

The maximum local background value for beryllium was 0.53 milligrams per kilogram (mg/kg). Beryllium was not detected above 0.53 mg/kg at site 235. Mercury, selenium, silver, and chromium⁺⁶ were not detected at Site 235. Other metal concentrations were below UTLs except one analysis for cadmium, vanadium, and zinc, and two analyses for iron. Sample 235-01-B had a cadmium concentration of 6.5 mg/kg, compared with a UTL of 3.82 mg/kg and a proposed Subpart S action level of 80 mg/kg. Sample 235-01-B had a vanadium concentration of 100 mg/kg, compared to a UTL of 40 mg/kg and a proposed Subpart S action level of 600 mg/kg. Sample 235-03-A had a zinc concentration of 80 mg/kg, compared to a UTL of 79 mg/kg and a proposed Subpart S action level of 20,000 mg/kg. Samples 235-01-A and 235-01-B had iron concentrations of 20,000 and 56,000 mg/kg, respectively, compared to a UTL of 16,962 mg/kg. No proposed Subpart S action level has been established for iron.

3.6.4 Radionuclides

Thallium was not detected at Site 235. Tritium, plutonium-239/240, and plutonium-238 were not detected above the minimum detectable activity (MDA). Uranium-238 and uranium-234 were detected in four samples at activities below the base-wide background 95th percentiles and below the maximum local background activity.

Uranium-235/236 was detected at 0.32 picocuries per gram (pCi/g) in Sample 235-03-A, compared to the base-wide background 95th percentiles of 0.168 pCi/g and a maximum local background activity of 0.33 pCi/g. Radium-226 was detected in Sample 235-01-A at 2.04 pCi/g compared to the base-wide background UTL of 1.94 pCi/g. Additional radiological analyses for radium-226 produced values less than 2.04 pCi/g.

3.6.5 Quality Assurance Results

As discussed in the Confirmatory Sampling and Analysis Plan (Appendix A), quality assurance samples, including field duplicates, trip blanks and rinsates, were collected as part of the 11-site sampling program. Analyses indicate that the field soil duplicates were comparable to the original soil sample results. The trip blanks and rinsates indicated no significant sampling contamination. QA results can be found in Appendix B. Level I and Level II data verification was conducted on all data, as described in the PIP (SNL/NM 1994).

3.7 Risk Analysis

To further evaluate the metals data for metals with concentrations greater than background UTLs, risk was analyzed for a combination of cadmium, iron, vanadium, and zinc, assuming the maximum detected concentrations. To further evaluate the site data for radionuclides with activities above background UTLs, 95th percentiles, or those without background UTLs, risk was analyzed for the combination of uranium-235/236 and radium-226, assuming the maximum detected activities.

The risk calculations were designed to produce conservatively large estimates of hazard index and radioactive dose to counter uncertainties in the soil data. This approach facilitates the following decision regarding future activities at Site 235:

- If the conservative estimates based on the soil data result in an unacceptable hazard index (greater than 1) or dose (greater than 10 mrem/year), further investigation and/or remediation will be needed; or
- If the hazard index and dose estimates are acceptable, the potential for health hazards at the site is extremely low, and further actions will not be needed.

Hazard indices and radionuclide doses were computed using methods and equations promulgated in proposed RCRA Subpart S documentation (EPA 1990). Accordingly, all calculations were based on the assumption that receptor doses from both toxic metals and radionuclides result from ingestion of contaminated soil.

Calculation of hazard indices required values of oral reference doses (oral RfDs) for each of the metals. The RfD values for cadmium, vanadium, and zinc were taken from EPA's IRIS database (IRIS 1991). The RfD for iron is a provisional value provided by EPA Region VI personnel.

Similarly, calculation of radionuclide doses required values of dose conversion factors, which are used to convert radionuclide intakes (in units of pCi/year) into effective dose equivalents (in units of mrem/year). Published values of dose conversion factors (Gilbert et al., 1989) exist for uranium-235/236 and radium-226.

To assure that the computed hazard indices and doses were conservatively large, only the maximum observed concentration of each constituent at a site was employed. To consider combined effects, a hazard index was calculated as the sum of the individual metal hazard quotients and a radiological dose was calculated as the sum of the individual doses.

Following proposed Subpart S methodology, the equation and parameter values used to calculate the summed hazard index for toxic metals were:

$$HI = \sum_{i} [HSR(i) \times S(i)]$$

(1)

where:

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HI = total hazard index (dimensionless),
HSR(I) = hazard index-to-soil concentration ratio for the i<sup>th</sup> metal (kg/mg)

= \frac{1 \text{ x A}}{\text{RfD(i) x W}} \text{ x \frac{0.001 g}{mg}}

S(I) = soil concentration of the i<sup>th</sup> metal (mg/kg),
I = soil ingestion rate = 0.2 g/day,
A = absorption factor (dimensionless) = 1,
W = body weight = 16 kg, and
RfD(I) = oral reference dose for the i<sup>th</sup> metal (mg/kg-day).
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Risk assessment guidance, prepared by the U.S. Environmental Protection Agency (EPA, 1989), recommends that the total hazard index be less than one in order for a site to be considered a non-threat to human health.

Following proposed Subpart S methodology, the equation and parameter values used to calculate the summed radioactive dose was:

DOSE =
$$\sum_{i}$$
 [DSR(i) x S(i)]

(2)

where:

DOSE = total effective dose equivalent (mrem/	yr);
DSR(I) = dose-to-soil concentration ratio for the	e i th radionuclide
$(mrem/yr)/(pCi/g) = I \times DCF(I);$	
S(I) = soil concentration of the i th radionuclio	de (pCi/g);
I = soil ingestion rate = $0.2 \text{ g/day} = 73 \text{ g/}$	
$DCF(I)$ = dose conversion factor for the i^{th} radio	nuclide (mrem/pCi).

The PIP stipulates that, for the purpose of computing media action levels, the total radioactive dose at a site should not be greater than 10 mrem/year (SNL/NM 1994), which corresponds to a cancer risk of less that 10⁻⁶ excess deaths.

The input and results of the risk calculations are presented in Tables 2 and 3. The summed hazard index for metals is greater than one and the summed radioactive dose is less than 10 mrem/year. Therefore, the site is considered to be risk-free in terms of radionuclide contamination.

The cause for the excessive risk from metals is iron. Excluding iron and performing the risk calculation on cadmium, vanadium, and zinc produces calculated action levels higher than the highest observed concentrations.³ The two highest of the 24 local background analyses are in close proximity to Site 235. The site iron concentration exceeded the risk-based action level for only one of the six samples. This sample was collected close to the metal grate by the culvert under the access road to the KAFB solid waste landfill. This one anomalously high concentration (56,000 mg/kg at 235-01-B) is interpreted to be the result of rust spreading from the metal grate. Figure 1 shows the location of sample Bkg-11-B, which had an iron concentration of 16,000 mg/kg and Bkg-12-B, which had an iron concentration of 15,000 mg/kg.

The recommended daily allowance (RDA) for iron is 18 mg. Assuming consumption of 0.2 g/day of soil, an iron concentration of 90,000 mg/kg would be necessary to obtain the iron RDA from eating the 0.2 g/day of soil. Even the Site 235 anomalous concentration of 56,000 mg/kg is less than 90,000 mg/kg.

Considering the high background of iron by Site 235, that only one of six site samples for iron posed an excessive risk, the fact that the anomalously high sample is close to a rusting metal grate, and the fact that even the anomalous sample would not supply the RDA for iron, iron should not be considered to pose a human health and environmental risk at Site 235. Therefore, the site is considered to be risk-free in terms of metals contamination.

3.8 Rationale for Pursuing a Risk-Based NFA Decision

Surface and shallow subsurface soil samples were collected at the most likely locations of contamination. Three surface and three subsurface soil samples were collected along the northern side of the outfall. The soil results indicate that all concentrations are less than action levels except for iron. Considering the high background of iron by Site 235, that only one of six samples for iron posed an excessive risk, the fact that the anomalously high sample is close to a rusting metal grate, and the fact that even the anomalous sample would not supply the RDA for iron, iron should not be considered to pose a human health and environmental risk at Site 235.

In addition

• A site visit in 1993 by ER personnel confirmed the presence of a confined natural drainage with no discoloration in the soils.

à	Observed (mg/kg)-	Action level (mg/kg)
cadmium	6.5	24
vanadium	100	. 365
zinc	80	292

- In June 1994, a UXO/HE visual survey was conducted by KAFB Explosive Ordnance Division (EOD) and found no UXO/HE ordnance debris at Site 235 (SNL/NM 1994a).
- In September, 1994, as part of the surface soil sampling effort at Site 235, a surface radiation survey was conducted (SNL/NM 1994b). No surface anomalies were detected at Site 235.

4. Conclusion

Based upon the evidence cited above, ER Site 235 has no releases of hazardous waste or hazardous constituents that pose a threat to human health and/or the environment. Therefore, ER Site 235 is recommended for an NFA determination.

5. References

5.1 ER Site References

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Sandia National Laboratories/New Mexico (SNL/NM), 1994b. "Summary of Radiological Survey Results by SNL Dept. 7714 for ER Sites 50, 227, 229, 230-234," Sandia National Laboratories, Albuquerque, New Mexico.

5.2 Reference Documents

Sandia National Laboratories/New Mexico, February 1994. Draft "Program Implementation Plan for Albuquerque Potential Release Sites," Sandia National Laboratories, Albuquerque, New Mexico.

Department of Energy (DOE), September, 1987. "Comprehensive Environmental Assessment and Response Program, Phase I Installation Assessment Sandia National Laboratories - Albuquerque," Department of Energy Albuquerque Operations Office, Environmental Safety and Health Division, Environmental Program Branch, September 1987.

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U.S. Environmental Protection Agency (EPA), April 1987. "Final RCRA Facility Assessment Report of Solid Waste Management Units at Sandia National Laboratories, Albuquerque, New Mexico," Contract No. 68-01-7038, EPA Region VI.

5.3 Aerial Photographs

Ebert & Associates, Inc., November 1994. "Photo-Interpretation and Digital Mapping of ER Sites 7,16,45,228 from Sequential Historical Aerial Photographs."

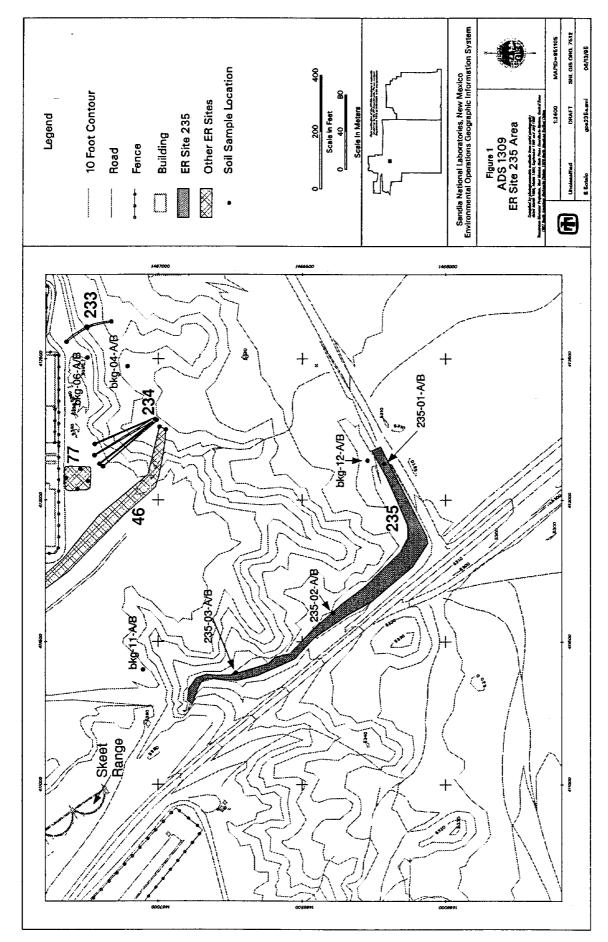


Figure 1. Storm Drain System Outfall Site 235.

Table 1. Site 235 - Results of Shallow Soil Sampling and Analysis

Sample Identifier	Analytical Method	Constituent	Concentration (mg/kg)	Qualifier(s)	Background (mg/kg)	Action Level (mg/kg)
235-01 - B	VOCs (8240)	Acetone	0.005	J		
235-01-B	VOCs (8240)	2-butanone	0.005	JB		
235-02-B	VOCs (8240)	2-butanone	0.006	В		
235-03-В	VOCs (8240)	2-butanone	0.004	JВ		
235-01-B	TAL Metals (6010)	Cadmium	6.5		3.82	80/2.4
235-01-A	TAL Metals (6010)	Iron	20,000		16,962	20,740
235-01-B	TAL Metals (6010)	Iron	56,000		16,962	20,740
235-01-B	TAL Metals (6010)	Vanadium	100		40	600/37
235-03-A	TAL Metals (6010)	Zinc	80		79	20000/29.6
235-03-A	Isotopic Uranium (HASL-300 4.5)	Uranium- 235/236	0.32 pCi/g		0.33/0.168 pCi/g	18.9 pCi/g
235-01-A	Gamma Spec- (in-house)	Radium-226	2.04 pCi/g	<u>.</u>	1.94 pCi/g	120 pCi/g

Notes

A "J" qualifier means detected at a concentration below the laboratory reporting limit.

A "B" qualifier means detected in the associated blank sample.

For the metals, background is the 95 percent upper tolerance level for the local background data.

For uranium-235/236, the first background value is the maximum of six local background values; the second value is the base-wide background 95th percentile.

For radium-226, background is the base-wide background 95th percentile.

The first action level for cadmium, vanadium and, zinc are proposed Subpart S levels.

All other action levels are risk-based levels.

Table 2. Metal Risk Calculations for Site 235

Constituent	Concentration (mg/kg)	RfD(I) (mg/kg- day)	Individual HI	Source of RfD
Cadmium	6.50E+00	1.00E-03	8.13E-02	IRIS
Iron	5.60E+04	3.00E-01	2.33E+00	Provisional RfD provided by EPA Region 6
Vanadium	1.00E+02	7.00E-03	1.79E-01	IRIS
Zinc	8.00E+01	3.00E-01	3.33E-03	IRIS
Summed HI			2.60E+00	

Table 3. Radionuclide Risk Calculations for Site 235

Constituent	Activity (pCi/g)	DCF(I) (mrem/pCi)	Individual Dose (mrem/year)	Source of DCF
Radium-226	2.04E+00	1.10E-03	1.64E-01	Gilbert et al., 1989
Uranium- 235/236	3.20E-01	2.50E-04	5.84E-03	Gilbert et al., 1989
Summed Dose			1.70E-01	

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APPENDIX A

Confirmatory Sampling and Analysis Plan

APPENDIX B

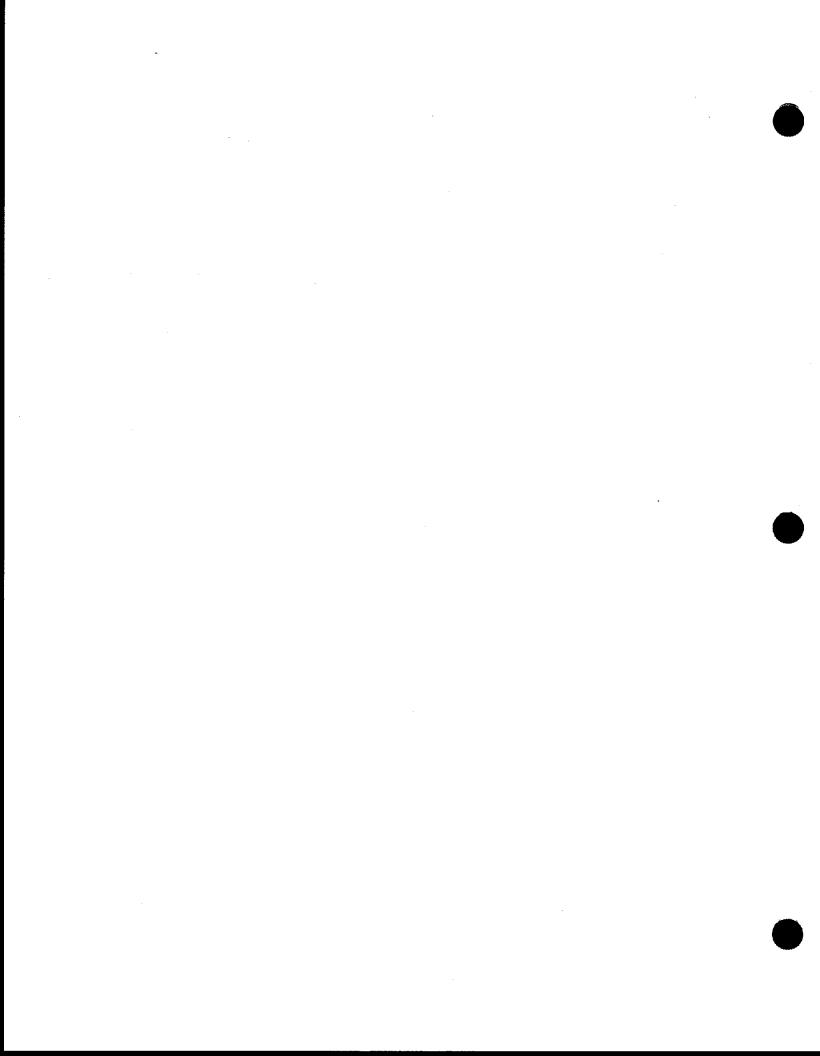
Analytical Results

APPENDIX C

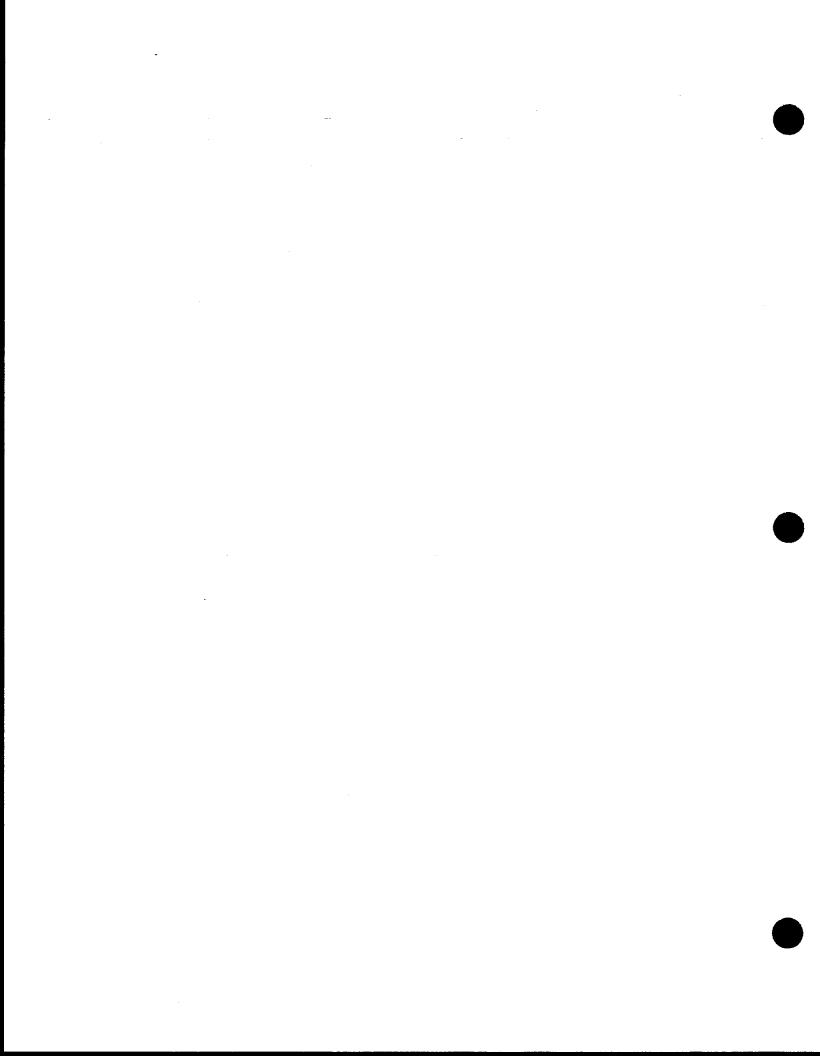
Background Calculations for Metals and Radionuclides

APPENDIX D

Probability Plots, Local Background UTL Calculations, and Base-wide Background UTLs for Radionuclides



Appendix A Confirmatory Sampling and Analysis Plan



SAMPLING AND ANALYSIS PLAN FOR ELEVEN SITES IN TIJERAS ARROYO OPERABLE UNIT SANDIA NATIONAL LABORATORIES/ NEW MEXICO

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Introduction

The purpose of the sampling and analysis described in this plan is to determine the appropriate way to proceed toward closure of 11 (of the 17) sites in the Tijeras Arroyo Operable Unit. Based on the surface and shallow subsurface soil samples and analyses for the constituents of concern (COCs), one of three approaches will be pursued for each site:

- A petition for "No Further Action" (NFA) will be produced for regulatory consideration;
- 2. A voluntary corrective measure (VCM) will be designed and implemented, hopefully followed by an NFA petition; or
- 3. The site assessment and eventual closure will follow the standard RFI/CMS path

Most of the sites covered by this Sampling and Analysis Plan (SAP) are outfalls from the storm water and sanitary sewer systems emanating from Sandia Technical Areas (TAs) I, II, and IV. The general sampling program for the outfalls will be to collect four samples at the head of the outfall, two samples of surface soil (0 to 6 inches deep) and two samples of shallow subsurface soil (18 to 36 inches deep) and four samples (two surface soil and two shallow subsurface soil) at the furthest extent of channel erosion and scour. The analytes for most of the samples are volatile organic compounds, semi-volatile organic compounds (BNAs), metals, chromium⁺⁶, for samples where chromium is found in a metals analysis, total petroleum hydrocarbon (TPH), explosives, Total Kjeldahl Nitrogen (TKN), nitrate/nitrite, and Gamma Spectroscopy for radionuclides, isotopic uranium, isotopic plutonium, tritium, and chlorodiphenyls (PCBs).

Sampling Procedures and Volumes

Surface soil samples will be collected with a stainless steel scoopula or trowel and placed in a stainless steel bowl. After at least 1000 ml¹ of soil has been collected, the soil will be thoroughly mixed in the bowl and transferred to two or three 500-ml sample bottles with a stainless steel scoopula. Sample bottles will be labeled accordingly and the appropriate sample information (sample depth, collection date and time, etc.) will be documented on the chain-of custody (COC) after each sample is collected. Samples will then be packaged and cooled to 4 degrees Celsius.

Shallow subsurface soil samples (18-36 inches) will be collected with a 2-inch (minimum) hand auger. A soil sample is collected by turning the auger clockwise and advancing it into the ground until the bucket at the end of the auger (last 6-8 inches) is full of soil or refusal occurs. Several runs with the auger is anticipated in order to obtain the appropriate volume. A hand shovel may also be used to bypass large rocks in order to continue with the auger. The auger is then extruded counter-clockwise from the ground and the soil is removed from the auger and placed in a stainless steel bowl. After 1,125² ml of soil has been collected, the soil will be mixed in the bowl and transferred to two or three 500-ml sample bottles and one 125-ml sample bottle with a stainless steel scoopula. Sample bottles will be labeled accordingly and the appropriate sample information will be documented on the COC after each sample is collected. Samples will then be packaged and cooled to 4 degrees Celsius.

Waste Generation and Equipment Decontamination

Decontamination of sampling equipment will be done between each sample.

Decontamination will include thoroughly washing the inside and outside of the sampling equipment with a spray of ALCONOX™ or LIQUINOX™ and water; rinsing with distilled,

¹The sample volume varies between 1,000 and 1,500 ml depending on the analyses for the sample.

²The sample volume varies between 1,125 and 1,625 ml depending on the analyses for the sample.

deionized water; and drying before reusing. No soil waste will be generated. The soil removed from the hand-auger holes, while collecting samples at a depth of 18 to 36 inches, will be return to the hole. The sampling tools, which are scoopulas/trowels, hand-augers, and shovels, will be decontaminated with water and ALCONOX™ after each use. The decon leachate will be stored in capped 1-gallon containers. One or two containers will be used for each site and two to four containers will be used for the background samples. The containers will be labeled as "IDW" and the site number identified on each container. All the containers will be stored at Site 232, a central location. The leachate waste will be disposed according to the analytical results of the soil samples collected at the site.

Site Descriptions

The sites that will be sampled are

- Site 46, Old Acid Waste Line Outfall;
- Site 50, Old Centrifuge Site;
- Site 77, Oil Surface Impoundment;
- Site 227, Bldg. 904 outfall;
- Site 229, Storm Drain System Outfall;
- Site 230, Storm Drain System Outfall;
- Site 231, Storm Drain System Outfall;
- Site 232, Storm Drain System Outfall;
- Site 233, Storm Drain System Outfall;
- Site 234, Storm Drain System Outfall; and
- Site 235, Storm Drain System Outfall.

The site locations are shown in Figure 1. A description of the site history, conditions, previous investigations, and sampling plans are described in the following sections.

Site 46: Acid Waste Line Outfall

The Old Acid Waste Line carried wastes from several buildings in TA I. The waste line begins as a north-south trending, 750-feet long open trench in a grassy field northwest of Building 981-1 in TA IV. No pipe opening is visible at the "head" of the trench. As the trench crosses the field, it turns to the southeast and continues to a non-engineered spillway at the edge of Tijeras Arroyo. The spillway lies on a bank (40 to 50 feet of relief) composed of compacted alluvial sediment. Historical aerial photographs show vegetation, presumably supported by the discharge, growing southeast of the spillway to the active arroyo channel (about 200 feet distance from the spillway). The site is not restricted and is easily accessible.

During use, discharged effluent averaged an estimated 130,000 gallons per day. Use of the line has been discontinued. The line received wastes from plating, etching, and photo processing operations, and cooling tower "blow down". Acids and metals are target contaminants. Chromic acid and ferric chloride are mentioned specifically in the site history, and ferric chloride was found in the soils during a limited sampling event. Various radionuclides, possibly including tritium, uranium, and plutonium were used in TA I.

Building 863 was a source of discharge to the Acid Line. The information sheet for ER Site 98 (Building 863, TCA Photochemical Release: Silver Catch Boxes) indicates the presence of trichloromethane, silver, and photo-processing chemicals with an ammonia-like odor. The waste solution from the silver recovery unit reportedly was discharged to the Old Acid Waste Line, which is the only specific information about chemical discharges.

The site has been visually surveyed for surface indications of unexploded ordnance and high explosives (UXO/HE). No UXO/HE were found. Also, a surface radiation survey was

conducted on the entire site. No surface radiation anomalies were detected.

The sampling program includes four samples collected at the "head" of the site outfall (by the fire extinguisher training area west of TA IV) and four samples collected by the spillway into the Tijeras Arroyo drainage (Figure 1). Every sample will be analyzed for tritium, metals, chromium *6 (if chromium is detected), TKN, and nitrate/nitrite. Half the samples will also be analyzed for semi-volatiles and cyanide. Additionally, all the subsurface samples will be analyzed for volatiles. The analytes are listed in Table 1. A "4" on the table indicates that ALL the samples will be analyzed

for that specific analyte whereas a "2" on the table indicates half the samples will have additional analyses for the analyte listed.

Site 50: Old Centrifuge

Site 50, Old Centrifuge, was an outdoor, rocket propelled centrifuge that was used in the early 1950s to test units under G forces. The facility is located east of the TA II fence in a slight depression on top the escarpment northwest of Tijeras Arroyo. The concrete centrifuge pad has a diameter of 80 to 90 feet. The site has a 7-foot high wooden retaining wall on the north, east, and south sides. The west side is open. The centrifuge arm assembly, which has a 20-foot radius, is sitting outside the wall to the north and appears to be intact. Control wiring to the center axis of the centrifuge was suspended from a cable between two telephone poles on the north and south side of the pad. The control wiring went to a bunker located to the southwest over the escarpment. The bunker had a electrical transformer containing PCB. The electrical transformer has been removed. The pad was not stained and no spills or leaks were reported.

The centrifuge was rocket driven by two T40 6-KS-3000 or two Deacon 3.5DS-5700 solid rocket motors. The combustion byproducts produced by these rocket motors were carbon dioxide, carbon monoxide, water, hydrochloric acid, aluminum oxide, and possibly barium oxide. No other HE is known or suspected at the site. The rocket orientation would expel combustion byproducts towards the retaining wall and the opening to the west. The rocket propellant would be consumed in the rocket motor case. Under normal operating conditions, no unburned propellant would be released.

In 1987, a reconnaissance investigation at five potential contaminated sites, including the Old Centrifuge Site, was conducted by the ER Project. Samples were analyzed for uranium, TNT, HSL inorganics, TCLP constituents, and EP Toxicity constituents. Metals, including barium, were detected at concentrations well below regulatory action levels. Total uranium concentrations were typical of area background levels. TNT, pesticides, PCBs, herbicides, and semi-volatiles TCLP compounds were not detected.

Prior to sampling, the surface will be surveyed for radiation. If contamination exists, it is expected to be around the edge of the centrifuge pad at the surface, probably along the open west side. The constituents of concern are metals (specifically lead, beryllium, and barium), depleted uranium, and high explosives. Four surface samples and four subsurface samples will be collected. The sampling locations will be biased toward the west side of the site because that is the open side (Figure 1). All surface samples will be analyzed for all the COCs. One-half of the subsurface samples will be analyzed for uranium and high explosives. All four subsurface samples will be analyzed for metals.

Site 77: Oil Surface Impoundment

The Oil Surface Impoundment Site is outside the TA IV fence, southeast of Building 981-1. The surface impoundment, which was constructed in the 1970's, is used to catch waste water from accelerators. At the time of the RCRA facilities environmental survey, the impoundment was unlined. Since then the impoundment was drained. Soil samples were analyzed for PCBs and

solvents. Based on the analytical results, the impoundment was determined to be clean. Subsequently, the impoundment was lined with geotextile and is now regulated under Sandia's Surface Water Discharge Program.

This site will not require UXO/HE or radiation surface surveys. Minimal confirmation sampling and analysis is proposed to verify that the site is clean. Three surface and three shallow subsurface samples are proposed. The samples will be collected along the perimeter of the existing lined pond (Figure 1). All the samples will be analyzed for PCBs. The subsurface soil samples also will be analyzed for volatile organic compounds (Table 1).

Site 227: Bunker 904 Outfall

Site 227 is an inactive outfall from the septic system for Building 904 (ER Site 48) in TA II. The site starts where the discharge exits the septic tank piping system, approximately 100 feet northeast of the southernmost point of TA II. The extent of the area influenced by the discharge may include the bank of Tijeras Arroyo below the outfall and some area between the outfall and the main channel of Tijeras Arroyo. The site is along the eastern edge of ER Site 45.

Building 904, built in 1948, was used for weapons assembly, HE testing, photo processing, and various other testing. Sanitary wastes were discharged to a septic tank, and other wastes were discharged to the outfall.

Mineral oil is also being considered a potential soil contaminant at all outfalls along the Tijeras Arroyo due to a recent release (June 1994) of mineral oil at Outfall 232 and vague historical records.

Possible soil contaminants are explosives, radioactive materials from weapons processing, including tritium, uranium, and plutonium, solvents (acetone, methylene chloride, methyl ethyl ketone, carbon tetrachloride, toluene, xylene, hexane, alcohols), and inorganics (ammonium hydroxide, barium, cadmium, silver, chromium, titanium, cyanide).

Access to this site is along the TA II perimeter road. This site is within the TA II testing exclusion zone. The best days to sample are generally Friday, Saturday, and Sunday, when testing ceases. Bruce Berry (telephone 845-8018) must be contacted to gain permission and access to this site. Prior to sampling

- tumbleweeds will be cleared from locations to be sampled and placed adjacent to the drainage;
- 2. these locations will be visually scanned for UXO/HE; and
- 3. these locations will be screened for surface radiation anomalies.

The proposed sampling program is to collect four surface soil samples and four shallow subsurface samples. Two surface and two subsurface samples will be collected at the outfall. The other two surface and two subsurface samples will be collected at the furthest visible channel erosion and scour (Figure 1). The analytes are listed in Table 1.

Sites 229 - 235: Storm Drain Systems Outfalls

These sites consist of the discharge areas at seven outfalls along the northern embankment of Tijeras Arroyo. The outfalls discharged industrial effluent and storm water from TAs I, II, and IV. Presently they only discharge storm water. The outfalls receive runoff from Site 96 (Storm Drain System) and other engineered drain systems within the three TAs. The sites are along approximately ¼ miles of the embankment.

The specific constituents in the industrial effluent at these sites are not known. The possible discharged contaminants include chromates, antifoulants, chromium, sodium hydroxide, hydrochloric acid, chromosulfuric acid, diesel, and other petroleum products. To cover this array of possible contaminants, soil samples will be analyzed for volatiles (subsurface samples only), semi-volatiles, metals and chromium⁺⁶, if chromium is found in the metals analysis.

Mineral oil is also being considered a potential soil contaminant at all outfalls along the Tijeras Arroyo due to a recent release (June '94) of mineral oil at Outfall 232 and vague historical records. Therefore, soil samples will also be analyzed for TPH.

At Sites 229 through 234, prior to sampling

- tumbleweeds will be cleared from locations to be sampled and placed adjacent to the drainage;
- 2. these locations will be visually scanned for UXO/HE; and
- 3. these locations will be screened for surface radiation anomalies.

Site 229 is due east of the footings of the old guard tower and the south "corner" of the TA II fence. It discharges near the top of the embankment through the center of ER Site 45. Access to this site is along the TA II perimeter road. This site is within the TA II testing exclusion zone. The best days to sample are generally Friday, Saturday, and Sunday, when testing ceases. Bruce Berry (telephone 845-8018) must be contacted to gain permission and access to this site. Because this site discharges from TA II, various radionuclides, possibly including tritium, uranium, and plutonium are of concern. Four surface soil and four subsurface soil samples will be collected at this site (Figure 1). The analytes are listed in Table 1.

Site 230 is west of Building 970 in TAIV. A drain pipe discharges into a bowl-shaped concrete structure adjacent to Building 970A. Flow from this structure is directed to a drain and flume located approximately 120 feet further west. The flume carries the flow to a discharge point slightly above the base of the arroyo embankment. Doug Bloomquist (845-7455) must be contacted to ensure that no laser testing is being performed in the area. Four surface soil and four subsurface soil samples will be collected at this site (Figure 1). The analytes are listed in Table 1.

Site 231 is west of Building 970 in TA IV. A drain pipe discharges to a concrete flume near the top of the embankment. The flume carries the flow to a discharge point near the base of the slope. Doug Bloomquist (845-7455) must be contacted to ensure that no laser testing is being performed in the area..Four surface soil and four subsurface soil samples will be collected at this site (Figure 1). The analytes are listed in Table 1.

Site 232 consists of two outfalls. One outfall is south of Building 970A, east of the lined lagoon. A drain pipe discharges to a concrete flume near the top of the embankment. The flume carries the flow to at discharge point near the bottom of hillside. On June 1, 1994, about 150 to 350 gallons of mineral oil was spilled into this outfall through the storm water drain by building 986. The day after the spill the site was screened for radiation and UXO/HE. No surface radiation anomalies or UXO/HE were found. Also, four surface soil and four subsurface soil samples were collected. The samples were sent to Quintera Laboratory in Denver for analysis for organics, metals, chromium¹⁶, and gamma spec. Other than TPH from the mineral, no contaminants were detected. A Voluntary Corrective Measure was conducted in July and August to remove soil contaminated with mineral oil above 100 mg/kg of TPH.

The second outfall in Site 232 also is south of Building 970A, west of lined lagoon, and approximately 120 feet east of the other Site 232 outfall. Discharge occurs from a concrete structure opening near base of embankment. Access to the site is along the road outside the south side of TA IV. Four surface soil and four subsurface soil samples will be collected at this drainage Figure 1). The analytes are listed in Table 1.

Site 233 is south-southwest of Building 986. Near the top of an escarpment, a small metal drain pipe discharges to an open drain which directs flow within another pipe before discharging near the base of the hillslope. Access to the site is along the road outside the south side of TA IV. Four surface soil and four subsurface soil samples will be collected at this site (Figure 1). The analytes are listed in Table 1.

Site 234 is southeast of Building 981I (Inflatable Building) and a lagoon impoundment (Site 77).

The site discharges into a steep-sided, deeply incised channel cut into the hillside. The drainage channel splits directly uphill of a tree. Access to the site is along the road outside the south side of TA IV. Both channels will be sampled. Six surface soil and six subsurface soil samples will be collected at this site (Figure 1). The analytes are listed in Table 1.

Site 235 is immediately downstream of a large concrete spillway on the northeast side of Pennsylvania and south of the Skeet Range, at the point where the road comes off the north bank of the arroyo and descends into the channel. The flow moves in a confined channel after dropping down the spillway. The site has been cleared for visible surface UXO/HE and screened for surface radiation with no anomalies detected. This channel is considerably larger than the other outfall sites. Six surface soil and six subsurface soil samples will be collected at this site (Figure 1). The analytes are listed in Table 1.

Background

Background soil concentrations for organic contaminants should be negligible. Background concentrations for total metals and radionuclides must be determined for comparison to concentrations found at the sites. Twelve locations have been identified to collect samples for background determination (Figure 1). At each of these sites, one sample will be collected at a depth of 0-6 inches and a second sample collected at 18-36 inches (Table 1)... In addition, the background study report prepared by International Technology Corporation (May 1994) will also be used to evaluate the data.

Quality Assurance

As shown in Table 1, quality assurance samples will include the following:

 Field "duplicates" on more than 10 percent of the samples. These samples will be collected adjacent to the original surface soil sample and in the same hole as the original subsurface soil sample;

Field soil blanks for more than 10 percent of the VOC analyses. These sample will be obtained from Sample Management Office (SMO) and will contain no VOCs; and

One rinsate blank. All rinsate will be composited in one container. A sample of the rinsate will be analyzed for all constituents. The disposal method for the rinsate will be determined by the analytical results on this sample.

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Appendix B Analytical Results

ACRONYMS FOR ANALYTICAL DATA

Organic/metals data for soil = mg/kg Radionuclides data for soil = pCi/g

ND = Not detected

NS = Not significant

MDA = Maximum Detectable Activity

J = Detected at a concentration below the laboratory reporting limit

B = Detected in the associated blank sample

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Concentrations in mg/kg
Activities in pCi/g
Sample Identifier XX-XX-A - surface soil samples
Sample Identifier XX-XX-B - subsurface soil samples

Quality Assurance Results for Organic Constituents

	НЧТ		I					QN	9														2
	total-Xylenes																						0.001 J
	Styrene																					0.001	
	Ругеле	0.040 J						0.19 J	0.28 J														
	Рћепалtћгепе	0.055 J	0.051 J					0.17 J	0.18 J														
	Methylene Chloride											 								0.003			
lituents	Fluoranthene	0.066 J	0.038 J					0.23 J	0.20														
Const	Di-n-octyl phthalate													0.16 J									
Organic	Сһгуѕепе							0.11 J	0.12 J							-							
ilts for	Benzo(b)fluoranthene							0.16 J	0.16 J	ļ													
ce Resu	Benzo(a)pyrene							0.050 J	0.092 J														
uality Assurance Results for Organic Constituents	Benzo(a)anthracene							0.071 J	0.006														
Quality,	ənoləsA				0.006 J													0.019	0.015			0.015	0.010
	4-Methyl-2-pentanone			0.001 J										_				0.002 J					
	2-Hexanone																	0.003 J		<u> </u>			
	2-Buťanone			0.007 J	0.006 J	0.004 J	0.005 J			0.006 J	0.006 J	0.006 J	0.006 J	0.003 JB		0.006 JB	C.004 JB	0.010B	0.009 JB	0.004 JB	0.007 JB	0.007 JB	0.005 JB
	Sample Type	original	duplicate	original	duplicate	original	duplicate	original	duplicate	trip blank	trip blank	trip blank (trip blank (trip blank (rinsate (
	Sample Identifier	227-01-A	227-01-A	227-01-B	227-01-B	227-04-B	227-04-8	229-01-A	229-01-A	229-02-B	229-02-B	229-03-B		230-04-B	230-04-B	235-02-B		Site 227	-	Site 230	232	234	Site 235

Quality Assurance Results for	Inorganic and Radiological Constituents

Section Color Co		,	· · · · · · · · ·				uito it	<u>yı morê</u>	janic a	mu reac	atotog	ical Co	nstit	uents	S			
227-02-A duplicate 6500 11 1.4 150 0.25 2.5 6.4 4.1 13 14000 9.1 170 ND 5.9 28 51 227-03-B original 5100 8.8 0.92 140 ND 2.1 5.9 4.5 11 13000 7.5 200 ND 5.4 25 48 227-03-B duplicate 6400 9.9 5.6 140 0.25 2.9 7.4 4.6 10 16000 8.9 230 ND 5.9 33 50 229-04-A original 8100 13 5.7 150 0.32 2.3 8.0 4.2 7.9 13000 12 210 ND 6.3 24 55 230-04-B original 1500 3.3 1.6 130 ND 0.61 2.3 ND 18 3500 4.2 110 ND 8.0 9.1 82 230-04-B duplicate 2400 4.9 1.7 140 ND 0.68 3.1 2.5 15 4500 4.1 120 ND 3.0 9.1 82 235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.4 22 66 50-01-B original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 4.5 17 18 50-02-A original 6400 13 5.7 210 0.53 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37 Bkg-05-A duplicate 5900 12 7.6 190 ND		Sample				<u> </u>		Cadmium	Chromium	Cobalt	Copper	Iron	Lead	Manganese	Mercury	vickel	/anadium	linc
227-03-B original 5100 8.8 0.92 140 ND 2.1 5.9 4.5 11 13000 9.1 170 ND 5.9 28 51 227-03-B duplicate 6400 9.9 5.6 140 0.25 2.9 7.4 4.6 10 16000 8.9 230 ND 5.4 25 48 229-04-A original 8100 13 5.7 150 0.32 2.3 8.0 4.2 7.9 13000 12 210 ND 6.3 24 55 230-04-B original 1500 3.3 1.6 130 ND 0.61 2.3 ND 18 3500 4.2 110 ND 8.2 24 52 230-04-B duplicate 2400 4.9 1.7 140 ND 0.68 3.1 2.5 15 4500 4.1 120 ND 3.4 9.7 71 235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 S0-02-A original 6400 13 5.7 210 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 S64 S65 S0-04-A original 6400 13 5.7 210 0.55 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37 S66-04 S									6.6		7.8	13000					_	51
227-03-B duplicate 6400 9.9 5.6 140 ND 2.1 5.9 4.5 11 13000 7.5 200 ND 5.4 25 48 227-03-B duplicate 6400 9.9 5.6 140 0.25 2.9 7.4 4.6 10 16000 8.9 230 ND 5.9 33 50 229-04-A original 8100 13 5.7 150 0.32 2.3 8.0 4.2 7.9 13000 12 210 ND 6.3 24 55 230-04-B original 1500 3.3 1.6 130 ND 0.61 2.3 ND 18 3500 4.2 110 ND 3.0 9.1 82 230-04-B duplicate 2400 4.9 1.7 140 ND 0.68 3.1 2.5 15 4500 4.1 120 ND 3.4 9.7 71 235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.3 14 10000 16 330 ND 8.9 22 37 Site 235 (insate ND									6.4	4.1	13	14000	9.1					1
229-04-A original 8100 13 5.7 150 0.32 2.3 8.0 4.2 7.9 13000 12 210 ND 6.3 24 55 229-04-A duplicate 7700 12 1.5 140 0.30 2.2 8.0 4.2 7.7 12000 11 190 ND 6.2 24 52 230-04-B original 1500 3.3 1.6 130 ND 0.61 2.3 ND 18 3500 4.2 110 ND 3.0 9.1 82 230-04-B duplicate 2400 4.9 1.7 140 ND 0.68 3.1 2.5 15 4500 4.1 120 ND 3.4 9.7 71 235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-01-B duplicate 3900 7.5 2.0 110 0.26 1.3 4.3 4.0 5.7 8800 5.9 150 ND 4.2 18 21 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 8kg-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.8 14 10000 16 330 ND 8.9 22 37 8kg-05-A duplicate ND)						_	5.9	4.5	11	13000	7.5	200	ND			
229-04-A duplicate 7700 12 1.5 140 0.30 2.2 8.0 4.2 7.9 13000 12 210 ND 6.3 24 55 230-04-B original 1500 3.3 1.6 130 ND 0.61 2.3 ND 18 3500 4.2 110 ND 3.0 9.1 82 230-04-B duplicate 2400 4.9 1.7 140 ND 0.68 3.1 2.5 15 4500 4.1 120 ND 3.4 9.7 71 235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A duplicate 5900 12 7.6 190 ND								2.9	7.4	4.6	10	16000	8.9	230				
230-04-B original 1500 3.3 1.6 130 ND 0.61 2.3 ND 18 3500 4.2 110 ND 3.0 9.1 82 230-04-B duplicate 2400 4.9 1.7 140 ND 0.68 3.1 2.5 15 4500 4.1 120 ND 3.4 9.7 71 235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 235-01-A duplicate 3000 5.3 1.3 160 ND 1.6 4.2 5.7 6.5 12000 9.4 180 ND 4.4 22 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.3 14 10000 16 330 ND 8.9 22 37 Site 235 ripsate ND								2.3	8.0	4.2	7.9	13000	12	210				
230-04-B original 1500 3.3 1.6 130 ND 0.61 2.3 ND 18 3500 4.2 110 ND 3.0 9.1 82 230-04-B duplicate 2400 4.9 1.7 140 ND 0.68 3.1 2.5 15 4500 4.1 120 ND 3.4 9.7 71 235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.4 22 66 50-01-B duplicate 3900 7.5 2.0 110 0.26 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.3 14 10000 16 330 ND 8.9 22 37 Site 235 rinsate ND		<u> </u>					0.30	2.2	8.0	4.2	7.7	12000	11					
235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 2001-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-01-B duplicate 3900 7.5 2.0 110 0.26 1.3 4.3 4.0 5.7 8800 5.9 150 ND 4.2 18 21 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A original 6400 13 5.7 210 0.53 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37 84g-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.3 14 10000 16 330 ND 8.9 22 37 816 235 ripsate ND	<u> </u>				1.6	130	ND	0.61	2.3	ND	18		4.2					
235-01-A original 3600 6.2 5.1 150 ND 2.7 6.0 8.4 6.6 20000 7.6 210 ND 4.5 36 66 205-01-A duplicate 3000 5.3 1.3 160 ND 1.6 4.2 5.7 6.5 12000 9.4 180 ND 4.4 22 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-01-B duplicate 3900 7.5 2.0 110 0.26 1.3 4.3 4.0 5.7 8800 5.9 150 ND 4.2 18 21 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A original 6400 13 5.7 210 0.53 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37 Site 235 ripsate ND				4.9	1.7	140	ND	0.68	3.1	2.5	15							
235-01-A duplicate 3000 5.3 1.3 160 ND 1.6 4.2 5.7 6.5 12000 9.4 180 ND 4.4 22 66 50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-01-B duplicate 3900 7.5 2.0 110 0.26 1.3 4.3 4.0 5.7 8800 5.9 150 ND 4.2 18 21 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A original 6400 13 5.7 210 0.53 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37 Site 235 ripsate ND					5.1	150	ND	2.7	6.0	8.4	6.6							_
50-01-B original 3100 6.5 2.1 110 0.25 1.3 4.1 3.9 6.2 7600 6.6 130 ND 4.5 17 18 50-01-B duplicate 3900 7.5 2.0 110 0.26 1.3 4.3 4.0 5.7 8800 5.9 150 ND 4.2 18 21 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A original 6400 13 5.7 210 0.53 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37					1.3	160	ND	1.6	4.2	5.7								_
50-01-B duplicate 3900 7.5 2.0 110 0.26 1.3 4.3 4.0 5.7 8800 5.9 150 ND 4.2 18 21 50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A original 6400 13 5.7 210 0.53 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37 Bkg-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.3 14 10000 16 320 ND 8.7 24 36	}				2.1	110	0.25	1.3	4.1	3.9								
50-02-A original 5800 12 4.2 220 0.38 1.6 5.2 4.3 12 6700 25 210 ND 7.1 11 69 50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A original 6400 13 5.7 210 0.53 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37 Site 235 ripsate ND			3900	7.5	2.0	110	0.26	1.3	4.3									
50-02-A duplicate 7000 14 6.4 280 0.55 2.2 8.3 6.1 17 9000 35 290 0.04 9.4 18 61 Bkg-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.3 14 10000 16 330 ND 8.9 22 37 Site 235 ripsate ND			5800	12	4.2	220	0.38	1.6	5.2					_				
Bkg-05-A original 6400 13 5.7 210 0.53 1.8 6.1 6.6 14 10000 16 330 ND 8.9 22 37 Bkg-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.3 14 10000 16 320 ND 8.7 24 36 Site 235 ripsate ND			7000	14	6.4	280	0.55	2.2										
Bkg-05-A duplicate 5900 12 7.6 190 0.50 1.7 6.0 6.3 14 10000 16 320 ND 8.7 24 36		original	6400	13	5.7	210	0.53	1.8										
Site 235 rinsate ND ND ND ND ND ND ND N		duplicate	5900	12	7.6	190	0.50										1	
	Site 235	rinsate	ND	ND	ND	ND	ND											

	r	Г							·	
Sample Identifier	Sample Type	TKN	NO ₃ /NO ₂	Potassium 40	Lead 212	Lead 214	Plutonium 239/240	Uranium 238	Uranium 235/236	Uranium 234
227-02-A		400	2.7					<u> </u>		
227-02-A		320	9.3				$\overline{}$			
227-03-A							0.004	0.4	0.15	0.61
227-03-A	duplicate							0.67	0.023	0.67
227-03-B	original							0.72	0.11	0.72
227-03-B	original	220	ND	-					0	0.12
227-03-B				27.8	0.71	0.7	 -			
227-03-B	duplicate	190	1.4							
229-01-A	original						0.007	0.45	0.17	0.67
229-01-A	duplicate							0.73	0.034	0.6
229-03-B	original							0.45	0.058	0.45
229-03-B	duplicate							0.99	0.06	1

Notes on Quality Assurance Data

Explosive residues were not detected in Site 50 duplicate sample

Hexavalent chromium was not detected in five duplicates and one decon rinsate

Cyanide was not detected in two duplicates and one decon rinsate

PCBs were not detected in one Site 77 duplicate sample

Tritium and Plutonium-238 were not detected in four duplicate samples

Selenium, silver, and thallium were not detected in any quality assurance samples

Appendix C Background Calculations for Metals and Radionuclides

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Appendix C. Background Calculations for Metals and Radionuclides

To evaluate metals data, 24 background samples were collected for metals analyses.⁴ Distribution analyses was performed first by constructing histograms. The histograms indicated a parametric distribution. Outliers were screened in a two-step process as described in the base wide background report (IT 1994). The first step is to perform an "a priori" screening for very high values relative to the rest of the data set. This is qualitatively performed by visually examining a column of sorted values. Maximum values that are a factor of 3 or 4 times higher than their nearest neighbor are removed from the data set during this step. None of the anomalous values were deleted by the "a priori" process.

The second step, from EPA, 1989, determines whether an observation that appears extreme fits the data distribution. A statistical parameter, T_n is calculated:

$$T_n = (X_n - X_a)/S$$

where:

 X_n = questionable observation;

X_a = sample arithmetic mean; and

S = sample standard deviation

T_n is compared to a table of one-sided critical values for the appropriate significance level (upper 5 percent) and sample size from a table provided in EPA 1989. Extreme concentrations for barium, calcium, chromium, copper and nickel were identified as outliers and were excluded from the data set. These anomalous values may have resulted from laboratory or sampling error.

Probability plots were then replotted to determine whether the data fit normal or lognormal populations. These plots are shown in Appendix D. The UTL⁵ was calculated for data sets that fit a normal or lognormal distribution. Data sets are provided in Appendix D. As recommended by EPA, a tolerance coefficient value of 95 percent was used (EPA 1989). Most metals background data fit lognormal distributions. Iron and zinc data fit normal distributions. UTLs were not calculated for mercury, selenium, and silver because mercury and selenium were not detected and silver was detected only once in the 24 background samples. The beryllium background data did not fit a normal or lognormal distribution. The maximum value in a data set is commonly taken as the UTL in a non-parametric setting (Guttman, 1970). The maximum background beryllium concentration was 0.53 mg/kg.

Base-wide background UTLs for radionuclides were established by International Technology (IT) Corporation to compare and evaluate radionuclide data (IT, 1994). A table is provided in Appendix D with radionuclide background data and the corresponding UTLs. The maximum activity from the six local background samples for isotopic plutonium and isotopic uranium was used as an additional

²These data are referred to as local background data. The data collected throughout Kirtland Air Force Base (KAFB), with most of the data collected within SNL/NM technical areas, are called base-wide background data (IT 1994).

 $^{^3}$ UTL = x + K·S, where:

UTL = Upper tolerance limit:

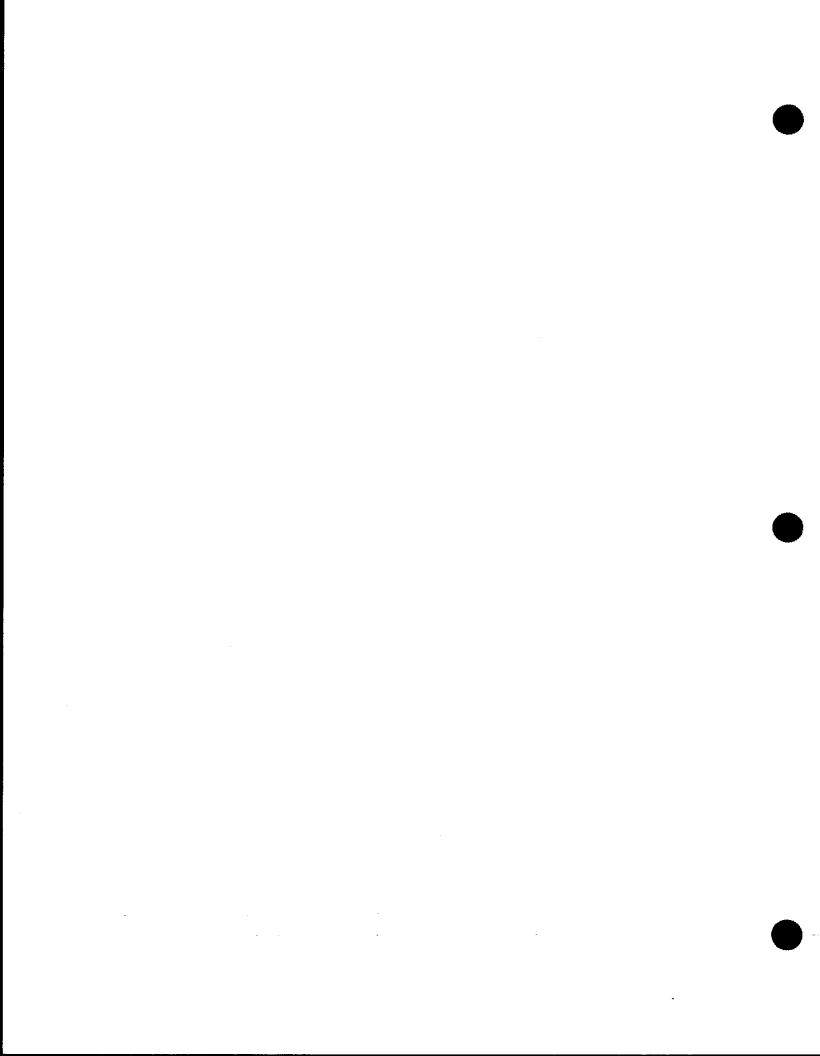
x = Sample arithmetic mean (for normal distribution), sample geometric mean (for lognormal distribution);

S = Sample standard deviation; and

K = One-sided normal tolerance factor (95 percent for these evaluations).

method to evaluate the data. Also, in-house gamma spectroscopy was performed on all 24 background samples and indicated low levels of radioactivity but no significant contamination.

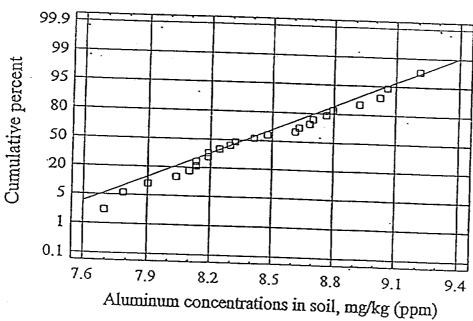
Appendix D Probability Plots, Local Background UTL Calculations, and BaseWide Background UTLs for Radionuclides



Summary Statistics for log(Aluminum) ht = 24 ecage = 0.42942 Median = 0.36529 Mode = Geometric mean = 8.41976 Variance - 0.170246 Standard deviation = 0.412609 Standard error = 0.0842235 Hinimum = 7.69621 Haximum = 9.21034 Range = 1.51(13 Lower quartile = 8.13153 Upper quartile = 8.73178 Interquartile range = 0.600253 Skewness = 0.132255 Stnd. skewness = 0.26451 Kurtosis = -0.792361 Stnd. kurtosis = -0.792361 Coeff. of variation = 4.89487

Sum = 202.306

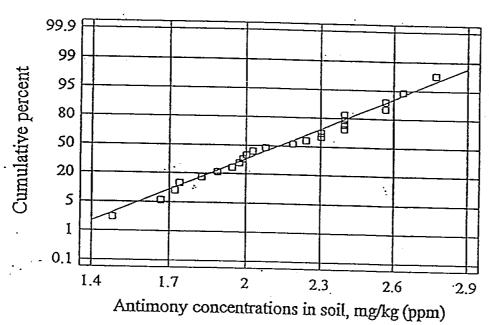
Lognormal Probability Plot for Aluminum



Summary Statistics for log(Antimony)

Count = 24 Average = 2.14609 Median = 2.13275 Mode = 2.3979 Geometric mean - 2.12004 Variance = 0.113831 Standard deviation = 0.337389 Standard error = 0.0608692 Minimum = 1.4816 Maximum - 2.77259 Range = 1.29098 Lower quartile = 1.91649 Upper quartile = 2.3979 Interquartile range = 0.481405 Skewness = -0.040772 Stnd. skewness = -0.0815441Kurtosis = -0.744171Stnd. kurtosis = -0.744171 Coeff. of variation = 15.7211 Sum = 51.5062

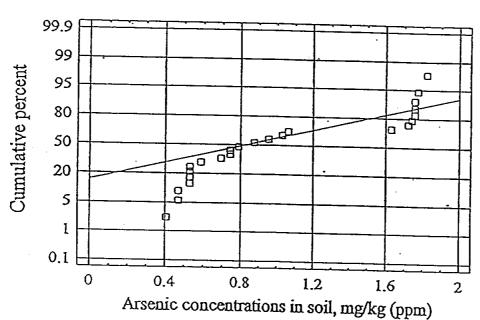
Lognormal Probability Plot for Antimony



Summary Statistics for log(Arsenic)

nt = 24 cage = 1.038 median = 0.031963 Mode = Geometric mean = 0.908119 Variance = 0.291153 Standard deviation = 0.539586 Standard error = 0.110143 Minimum = 0.405465 Maximum - 1.82455 Range = 1.41908 Lower quartile = 0.530628 Upper quartile = 1.73162 Interquartile range = 1.20099 Skewness = 0.463036 Stnd. skewness = 0.926071 Kurtosis = -1.58507 Stnd. kurtosis = -1.58507Coeff. of variation = 51.983 Sum = 24.9121

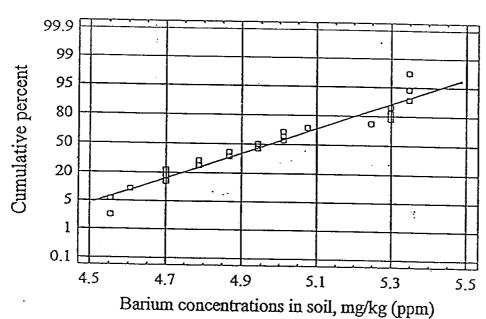
Lognormal Probability Plot for Arsenic



Summary Statistics for log(Barium)

Count = 23 Avecage = 4.96948 Median = 4.94164 Mode = 5.34711 Geometric mean - 4.96236 Variance = 0.0740602 Standard deviation # 0.27214 Standard error = 0.0567451 finimum = 4.55388
faxlmum = 5.34711 Range = 0.793231 Lower quartile = 4.70048 Jpper quartile = 5.29832 interquartile range = 0.597837 kewness = 0.0653415 itnd. skewness = 0.127931Turtosis = -1.30542 tnd. kurtosis = -1.27794beff. of variation = 5.47622 um = 114.298

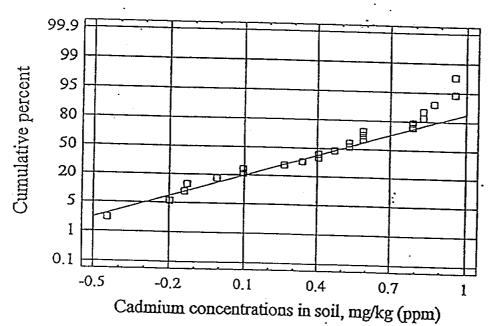
Lognormal Probability Plot for Barium



Summary Statistics for log(Cadmium)

punt = 24 erage = 0.416764 Median = 0.500316 Mode = Geometric mean = Variance = 0.159937 Standard deviation = 0.399922 Standard error = 0.0816337 Minimum = -0.446287 Maximum = 0.955511 Range = 1.4018 Lower quartile = 0.0953102 Upper quartile = 0.788457 Interquartile range = 0.693147 Skewness = -0.506707Stnd. skewness ≈ -1.01341 Kurtosis = -0.674504 Stnd. kurtosis = -0.674504 Coeff. of variation = 95.9587 Sum = 10.0023

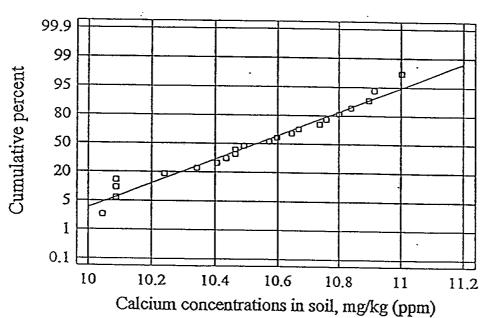
Lognormal Probability Plot for Cadmium



Summary Statistics for log(Calcium)

Count = 23Average = 10.5579 Median = 10.5713 Mode = 10.0058 Geometric mean = 10.5532 Vaciance = 0.10513 Standard deviation = 0.324237 Standard error = 0.0676081 Minimum = 10.0432 Maximum = 11.2645 Range = 1.22121 Lower quartile = 10.3417 Upper quartile = 10.7996 Interquartile range = 0.457833 Skewness = 0.109797 Stnd. skewness = 0.214971Kurtosis = -0.415646 Stnd. kurtosis = -0.406895Coeff. of variation = 3.07103 Sum = 242.832

Lognormal Probability Plot for Calcium



unt = 23

verage = 1.61041

Median = 1.79176

Mode =

Geometric mean = 1.55042

Variance = 0.204195

Standard deviation = 0.451079

Standard error = 0.0942233

Minimum = 0.693147

Maximum = 2.30259

Range = 1.60944

Lower quartile = 1.28093

Upper quartile = 2.00148

Interquartile range = 0.720546

Skewness = -0.274151

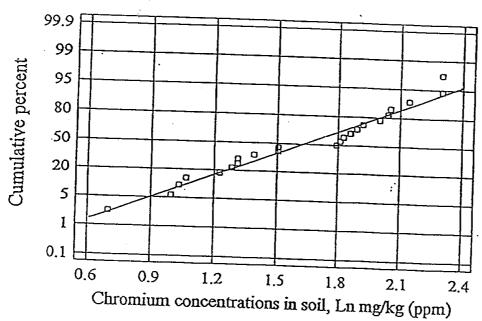
Stnd. skewness = -0.536757

Kurtosis = -0.905395 Stnd. kurtosis = -0.886332 Coeff. of variation = 27.9211

Sum = 37.2235

Summary Statistics for log(Chromium)

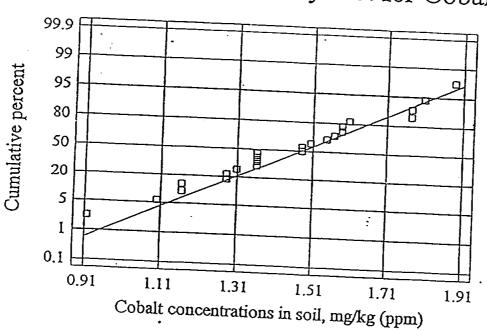
Lognormal Probability Plot for Chromium



Summary Statistics for log(Cobalt)

Count = 24 Average = 1.29969 Median = 1.42129 Mode = Geometric mean = Variance = 0.574775 Standard deviation = 0.758139 Standard error - 0.154754 Minimum = -2.07944 Maximum = 1.88707 Range = 3.96651 Lower quartile = 1.28093 Upper quartile = 1.58924 Interquartile range = 0.308301 Skewness = -4.13299Stnd. skewness = -8.26598 Kurtosis = 18.9091 Stnd. kurtosis = 18.9091 Coeff. of variation = 58.3324 Sum = 31.1925

Lognormal Probability Plot for Cobalt



Summary Statistics for log(Copper)

Mcd = 23

Median = 1.98787

Mode =

Geometric mean = 1.96762

Variance = 0.0713494

Standard deviation = 0.267113

Standard error = 0.0556969

Minimum = 1.43508

Maximum = 2.56495

Range = 1.12986

Lower quartile = 1.80829

Upper quartile = 2.17475

Interquartile range = 0.366463

Skewness = -0.263077

Stnd. skewness = -0.515077

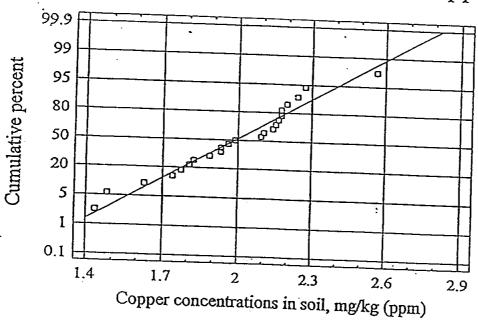
Kurtosis = 0.18883

Stnd. kurtosis = 0.184854

Coeff. of variation = 13.4528

Sum = 45.6679

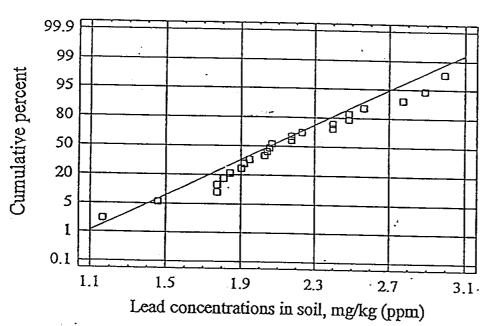
Lognormal Probability Plot for Copper



Summary Statistics for log(Lead)

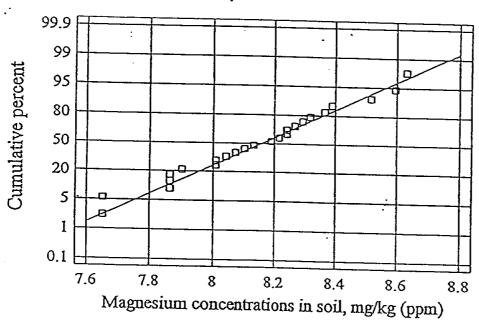
Average = 2.13936 Median = 2.06049 Mode = Geometric mean = 2.09509 Variance = 0.187882 Standard deviation = 0.433454 Standard error - 0.0884784 Minimum = 1.16315 Maximum = 2.99573 Range = 1.83258 Lower quartile = 1.87133 Upper quartile = 2.4414 Interquartile range = 0.570072 Skewness = 0.0350174 Stnd. skewness = 0.0700348 Kurtosis = 0.200156 Stnd. kurtosis = 0.200156 Coeff. of variation = 20.261 Sum = 51.3446

Lognormal Probability Plot for Lead



Summary Statistics for log(Magnesium) rage = 8.14232 Median = 8.16011 Mode = Geometric mean = 8.13815 Variance = 0.0706013 Standard deviation = 0.265709 Standard error = 0.0542376 Minimum = 7.64969 Maximum = 8.63052 Range = 0.980829 Lower quartile = 7.95369 Upper quartile = 8.3064 Interquartile range = 0.352709 Skewness = -0.0600481 Stnd. skewness = -0.120096 Kurtosis = -0.414246 Stnd. kurtosis = -0.414246 Coeff. of variation = 3.26331 Sum = 195.416

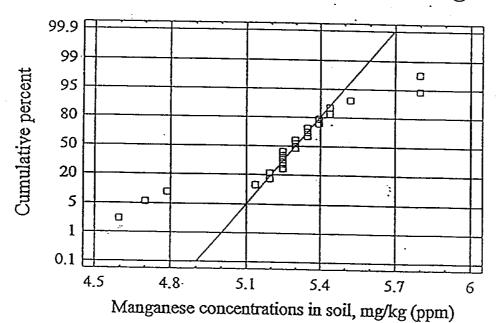
Lognormal Probability Plot for Magnesium



Summary Statistics for log(Manganese)

Count = 24 Average = 5.2733 Median = 5.29832 Mode = Geometric mean = 5.2661 Variance = 0.0771874 Standard deviation = 0.277826 Standard error = 0.056711 Minimum - 4.59512 Maximum - 5.79909 Range = 1.20397 Lower quartile = 5.21999 Upper quartile = 5.39363 Interquartile range = 0.173637 Skewness = -0.660387Stnd. skewness = -1.32077Kurtosis = 1.62566 Stnd. kurtosis = 1.62566 Doeff. of variation = 5.26854 Sum = 126.559

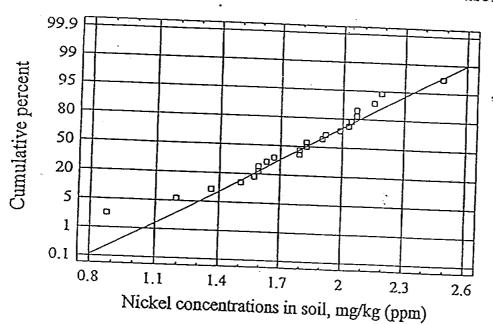
Lognormal Probability Plot for Manganese



Summary Statistics for log(Nickel)

punt 😐 23 recage = 1.70451 Median = 1.82455 Geometric mean - 1.74596 Variance = 0.1246 Standard deviation = 0.352987 Standard error = 0.0736029 Minimum = 0.875469 Maximum = 2.48491 Range = 1.60944 Lower quartile = 1.58924 Upper quartile = 2.04122 Interquartile range = 0.451985 Skewness = -0.609856 Stnd. skewness = -1.19403 Kurtosis - 0.992502 Stnd. kurtosis = 0.971605Coeff. of variation = 19.7806 Sum = 41.0438

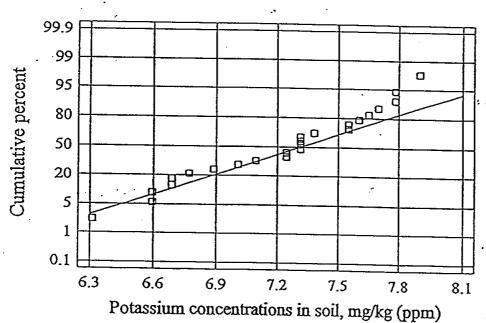
Lognormal Probability Plot for Nickel



Summary Statistics for log(Potassium)

Count = 24 Average = 7.21862 Median = 7.31322 Mode = 7.31322Geometric mean = 7.20542 Variance = 0.195599 Standard deviation = 0.442265 Standard error = 0.0902771 Minimum = 6.30992 Maximum = 7.90101 Range = 1.59109 Lower quartile = 6.82802 Upper quartile = 7.57526 Interquartile range = 0.747233 Skewness = -0.373735Stnd. skewness = -0.74747Kurtosis = -0.83864Stnd. kurtosis = -0.83864Coeff. of variation = 6.12673 Sum = 173.247

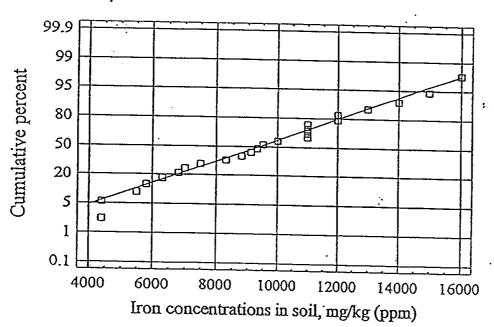
Lognormal Probability Plot for Potassium



Summary Statistics for Iron

punt = 24 verage = 9529.17 Median = 9400.0 Mode = 11000.0Geometric mean = 8977.5 Variance = 1.0363E7 Standard deviation = 3219.17 Standard error = 657.109 Minimum = 4400.0 Maximum = 16000.0 Range = 11600.0 Lower quartile = 6900.0 Upper quartile = 11500.0 Interquartile range = 4600.0 Skewness = 0.20025Stnd. skewness = 0.400499Kurtosis = -0.620589 Stnd. kurtosis = -0.620589Coeff. of variation = 33.7822 Sum = 228700.0

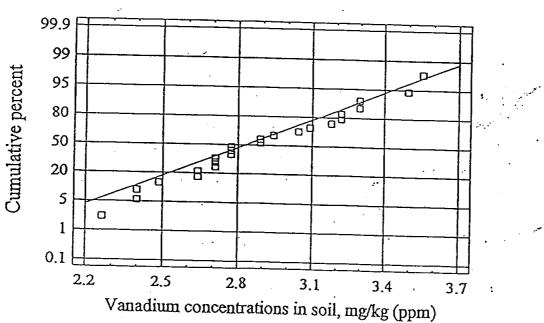
Normal Probability Plot for Iron



Summary Statistics for log(Vanadium)

Count = 24 Average = 2.89094 Median = 2.03148 Mode = Geometric mean = 2.87064 Variance = 0.122444 Standard deviation = 0.34992 Standard error - 0.0714271 Minimum = 2.26176 Maximum = 3.55535 Range = 1.29358 Lower quartile = 2.67355 Upper quartile = 3.19846 Interquartile range = 0.524911 Skewness = 0.158415 Stnd. skewness = 0.316831 Kurtosis = -0.688491 Stnd. kurtosis = -0.688491 Coeff. of variation = 12.104 3um = 69.3826

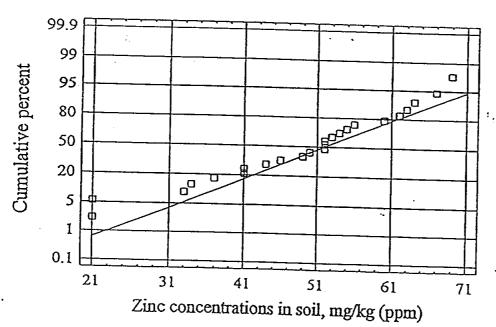
Lognormal Probability Plot for Vanadium



Summary Statistics for Zinc

erage = 49.0 dian = 52.0 Mode = 52.0 Geometric mean = 46.9434 Variance - 171.478 Standard deviation = 13.095 Standard error = 2.673 Minimum = 21.0 Maximum = 69.0 Range = 48.0 Lower quartile = 41.0 Upper quartile = 58.0 Interquartile range = 17.0 Skewness = -0.633044 Stnd. skewness = -1.26609 Kurtosis = -0.0224531 Stnd. kurtosis = -0.0224531 Coeff. of variation = 26.7244 Sum - 1176.0

Normal Probability Plot for Zinc



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Concentrations in mg/kg
Activities in pCi/g
Sample Identifier XX-XX-A - surface soil samples
Sample Identifier XX-XX-B - subsurface soil samples

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Lo	muibo2	QN	운	ΩN	QN	QN	480	QN	QN	QΝ	ΩN	QN	420	QN	380	Q N	430	280	640	ND	ND I	280	$\overline{}$	_	620
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	Sample Identifier	Bkg-01-A	Bkg-01-B	Bkg-02-A	Bkg-02-B	Bkg-03-A	Bkg-03-B	Bkg-04-A	Bkg-04-B	Bkg-05-A	Bkg-05-B	Bkg-06-A	Bkg-06-B	Bkg-07-A	Bkg-07-B	Bkg-08-A	Bkg-08-B	3kg-09-A	3kg-09-B	3kg-10-A	3kg-10-B	3kg-11-A	3kg-11-B	3kg-12-A	2Kg-17-B

Concentrations in mg/kg
Activities in pCi/g
Sample Identifier XX-XX-A - surface soil şamples
Sample Identifier XX-XX-B - subsurface soil samples

Normal Parameters for Tijeras Arroyo Local Metal Background Data Aluminum Antimony Manganese Cadmium Arsenic Barium Statistical Parameter median 4300 8.5 2 140 2 4.2 7.3 geometric mean 9400 7.9 4579.9 200 8.6 6.2 17 144 52 2 5 3.7 7.3 maximum 8977.5 8.5 195 10000 6 18 16 6 210 47 3 10 6.6 13 minimum 16000 20 2200 330 12 4.4 2 35 69 95 2 arithmetic average 4970.8 0.1 4.2 4400 3.2 99 2.4 9.6 3 149 21 2 5.5 standard deviation 4.2 7.5 9529.2 9.3 2095.4 202 6.3 3 19 2 40.5 49 2.3 1.3 normal tolerance 2 3219.2 4.2 2.309 53.6 2.1 2.3 6.9 13 2.33 2 2.3 2.3 2.3 2.309 UTL 2.3 2.31 4927.4 2.3 16 2.3 2.3 244 11 7.3 12 16962 19 326 35

Log	Inormai I	aran	nefei	e for T	::								-		-
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arithmetic average	8.4294	2.2	1	4.97	0		0	O	=	ورا	Σ	Nick	ā	Zinc	
standard deviation	0.4126	0.3	1	0.27	0	1.6	1.3		9.1025	2.1	5.27	1.8	2.9	3.8	
normal tolerance	2.309	2.3	2	2.33		0.5	0.8	0.3	0.3631	0.4	0.28	0.4	0.3	0.3	ı
UTL	9:38211				2	2.3	2.3	2.3	2.309	2.3	2.31	2.3	2.3		1
e ^{UTL}			2	5.6	1	2.7	3.1	2.6	9.941	3.1	5.91			2.3	
	11874	19	10	271	4	14	21	14				2.6	3.7	4.6	ı
							~'	- 4	20764	_23	370	14	40	98	

Insufficient data for mercury, selenium, silver, and thallium to calculate statistics

All concentrations in mg/kg



Summary of Background Concentrations for Radionuclides in Soil

Analyte	Original Number of Samples	Number of Detects	Number of Rejected Samples	Distribution	Ranga		Geometric Mean	· Value	95" Upper Tolerance	
Bismuth-212	324	12	200	1 Jp#	(bCNg)	·c	(pCVp)	(pCl/g)	(ocivo)	95" Percentile
Bismuth-214	340	200	700	Nonparametric	0.414-2.7	12	1,1055	0.		(600)
Cesium.137	200	176	-19	Nonparametric	0.27-1.4	321	0730	<u> </u>	-	2.7
(Surface)	905	261	26				0,040	9.0	•	9.0
(Subsurface)		1	ı	Nonparametric	0.004-101	، ج	1		,	
	ı	ı	ı	Unknown	-detection limit	172	0.200	0.2495	•	0.92
Coball-60	321	-			(<0.0686)		(<0.0686)	(40 OSB)	1	sdetection limit
	<u> </u>	-	74	Unknown	· «detection Ilmit	247	edataction limit	(DOCOLOT)		(<0.0686)
Lead-210*	338	40	660		(<0.0418)		(<0.0418)	(<0.0418)		sdetection limit
Lead-212"	323	222	. 755	Nonparametric	0.312.0	46	2,26838	2.835		(40.0418)
Lead-214*		202	05	Lognormal	0.1-1.4	233	0.40890		<u> </u>	6.8
	643	241	61	Lognormal	0.29=1.13	18	2000	6:5	1.0795	1
Polassium-40	722	720	7	I GENERAL MANAGEMENT	51.1-62.0	200	0.549	0.56	08.0	
Radium-224	24	24	0		0.182-31.0	718	15.889	16.4	25.34	
Radium-226	368	53	317	Nonparametric	0.43-0.97	77	0.6747	0.655		0.558
Radium-228	24	24		Lognormal	0.5-2.09	25	0.713	0.590	1.94	
Radon	0	0	c	Notiparametric	0.451,05	2	0.695	0.630		1.05
Stronthum-90	54	45) 0	Unknown		0	2	-	-	
Thorium-232	136	136		ronparameiric	0.0321.85	45	0.2528	0.2883		0.75.6
Thorium-234	365	5		Lognormal	0.23-1.20	136	0.7971	0.810	0363	3
Tritium		35	330	Lognormal	0.324~3.0	35	0.7796	2,20	967.	•
Iranium 20	0	0	0	Unknown	-	-	+		SB.7	:
	4	4	0	Nonparametric	0 2 2 0	. .	-		_	•
Uranium-235	95	21	75	Nonoarametric	0000	-	0.897	6.0	-	0.1
Uranium-238	223	206	17	╁	0.00-0.10	R I	0.1198	0.1235		0.168
Sample size.				\dashv	0.0033-2.065	508	0.506	0.763		1,1
These modificents are not listed as 000 to 17.	Co so polali soc v							7		

Sample size.
These consilvents are not listed as COC in Table 2.2 for this media.
Constituents of concern are of unknown distribution type because data are either below the limit of detection, unusable, or nonexistent.

(II) 1994)

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